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## AMENDMENTS TO THE CLAIMS

- 1. (Currently Amended) A method for influencing the traction or braking torque on at least one driving wheel of an industrial truck, the driving wheel being driven by a driving motor, wherein the slip between the driving wheel and the floor is measured or calculated by comparing the circumferential speed of the driving wheel and the measured travelling speed of the industrial truck, the such determined slip being compared with a predetermined value for the slip, and the absolute amount of the torque of the driving motor is reduced in dependence from the difference between the actual and the predetermined value for the slip through a slip controller if the actual slip exceeds the predetermined slip for the purpose of driving and/or braking it wherein the torque of a driving motor (30) for the industrial truck is reduced by means of a slip regulator (46) at an appropriate amount depending on the slip by determining the slip between the driving wheel (14) and the floor by making a comparison of the circumferential speed measured or calculated for the driving wheel (14) and the vehicle travelling speed measured for the industrial truck, and comparing it to a setpoint.
- 2. (Original) The method according to claim 1, characterized in that the driving motor (30) is an electric motor or hydraulic engine.
- (Original) The method according to claim 2, characterized in that a three-phase a.c. motor is provided.
- 4. (Currently Amended) The method according to claim 1, characterized in that the an intervention of the slip regulator (46) controller takes place behind in response to an rpm governor (24) which has a desired torque as an output and the output of which, after undergoing correction by the slip regulator controller, is fed to a secondary order torque regulation circuit.
- 5. (Currently Amended) The method according to claim 2, characterized in that the an intervention of the slip regulator (46) controller takes place behind in response to an rpm governor (24) which has a desired torque as an output and the output of which, after undergoing correction by the slip regulator controller, is fed to a secondary order torque regulation circuit.





- 6. (Currently Amended) The method according to claim 3, characterized in that the an intervention of the slip regulator (46) controller takes place behind in response to an rpm governor (24) which has a desired torque as an output and the output of which, after undergoing correction by the slip regulator controller, is fed to a secondary order torque regulation circuit.
- 7. (Original) The method according to claim 1, characterized in that the vehicle travelling speed is determined from the number of revolutions of at least one non-driven wheel (10, 12) of the industrial truck.
- 8. (Original) The method according to claim 2, characterized in that the vehicle travelling speed is determined from the number of revolutions of at least one non-driven wheel (10, 12) of the industrial truck.
- (Original) The method according to claim 3, characterized in that the vehicle travelling speed is determined from the number of revolutions of at least one non-driven wheel
   (10, 12) of the industrial truck.
- 10. (Original) The method according to claim 4, characterized in that the vehicle travelling speed is determined from the number of revolutions of at least one non-driven wheel (10, 12) of the industrial truck.
- 11. (Currently Amended) The method according to claim 1, characterized in that the speed is measured on two non-driven wheels (10, 12) in order to determine the a reference speed on the driving wheel (14) as a vector quantity [[(]]direction and magnitude[[)]] from the vehicle geometry.
- 12. (Currently Amended) The method according to claim 2, characterized in that the speed is measured on two non-driven wheels (10, 12) in order to determine the a reference speed on the driving wheel (14) as a vector quantity [[(]]direction and magnitude[[)]] from the vehicle geometry.
- 13. Currently Amended) The method according to claim 3, characterized in that the speed is measured on two non-driven wheels (10, 12) in order to determine the a reference speed on the driving wheel (14) as a vector quantity [[(]]direction and magnitude[[)]] from the vehicle geometry.



- 14. (Currently Amended) The method according to claim 4, characterized in that the speed is measured on two non-driven wheels (10, 12) in order to determine the a reference speed on the driving wheel (14) as a vector quantity [[(]]direction and magnitude[[)]] from the vehicle geometry.
- 15. (Currently Amended) The method according to claim 5, characterized in that the speed is measured on two non-driven wheels (10, 12) in order to determine the a reference speed on the driving wheel (14) as a vector quantity [[(]]direction and magnitude[[)]] from the vehicle geometry
- 16. (Currently Amended) The method according to claim 11, characterized in that a calculation of the <u>a</u> circumferential component and/or the <u>an</u> axial component of the reference speed is performed by measuring the <u>a</u> steering angle on the steered driving wheel (14).
- 17. (Currently Amended) The method according to claim 1, characterized in that the desired slip for a certain friction pairing is constituted by an optimum slip value.
- 18. (Currently Amended) The method according to claim 2, characterized in that the a desired slip for a certain friction pairing is constituted by an optimum slip value.
- 19. (Currently Amended) The method according to claim 3, characterized in that the a desired slip for a certain friction pairing is constituted by an optimum slip value.
- 20. (Currently Amended) The method according to claim 4, characterized in that the a desired slip for a certain friction pairing is constituted by an optimum slip value.
- 21. (Currently Amended) The method according to claim 5, characterized in that the a desired slip for a certain friction pairing is constituted by an optimum slip value.
- 22. (Currently Amended) The method according to claim 6, characterized in that the a desired slip for a certain friction pairing is constituted by an optimum slip value.
- 23. (Currently Amended) The method according to claim 7, characterized in that the a desired slip for a certain friction pairing is constituted by an optimum slip value.
- 24. (Currently Amended) The method according to claim 17, characterized in that the a desired slip is determined while the industrial truck is in operation.
- 25. (Currently Amended) The method according to claim 11, characterized in that the an



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axial speed component is determined from the reference speed of the steered driving wheel (14) and the steering angle is limited or reduced if the axial speed component exceeds a preset point.

26. (Currently Amended) The method according to claim 16, characterized in that the an axial speed component is determined from the reference speed of the steered driving wheel (14) and the steering angle is limited or reduced if the axial speed component exceeds a preset point.